

Sensitivity of the rf-set

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Low Temperature Laboratory

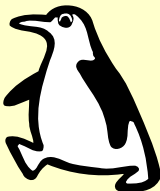
Helsinki University of Technology, Finland

Kevin Bladt and Per Delsing

Chalmers University of Technology, Sweden

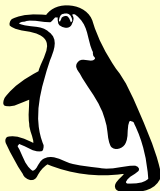
Konrad Lehnert, Lafe Spietz and Rob Schoelkopf

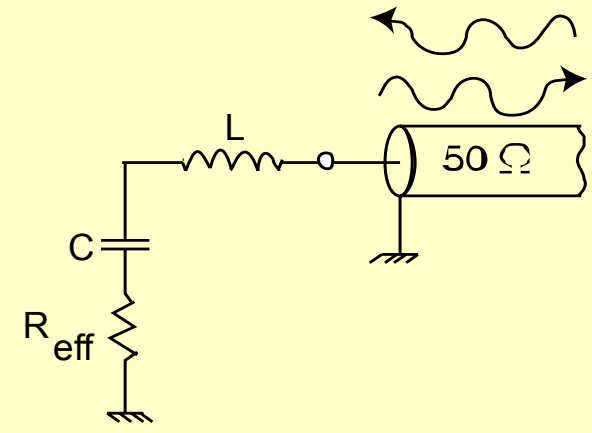
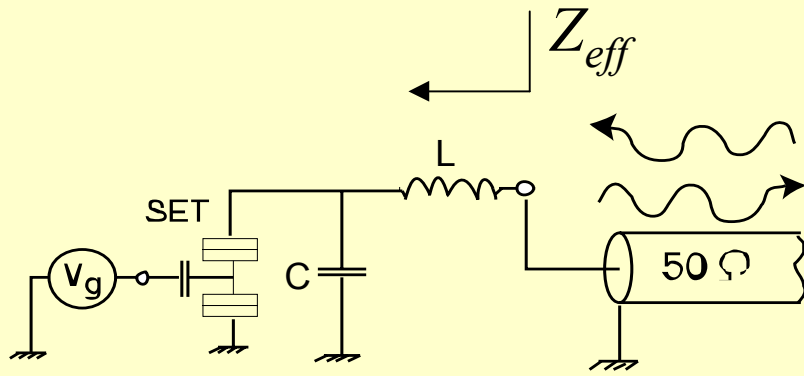
Yale University, USA



Outline

- short introduction to rf-SET
- Signal-to-noise ratio and SET charge sensitivity
- Noise power waves
- experimental verification





Reflected wave complex amplitude Γ

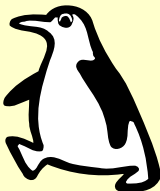
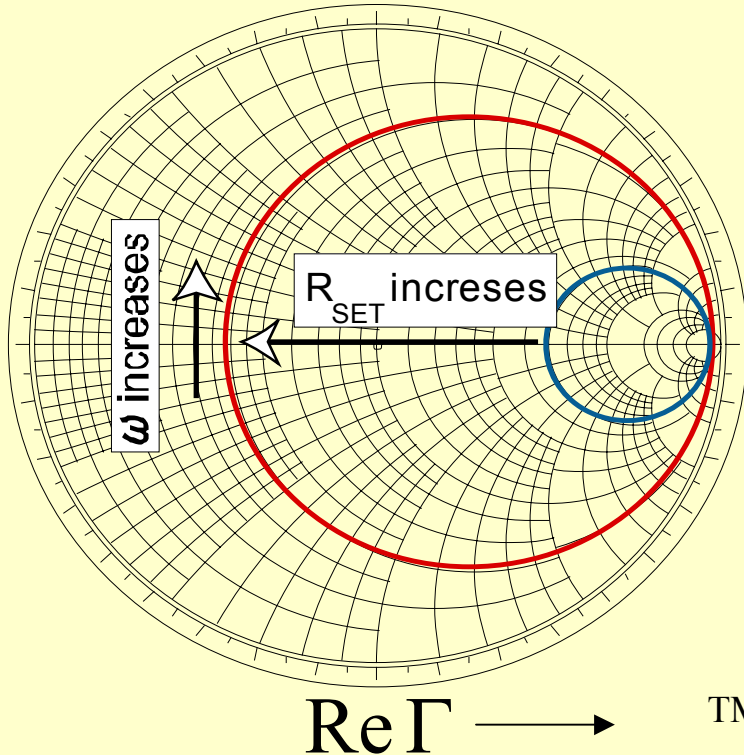
generally:

$$Z_{eff} = R_{eff} + j \frac{2Z_T \Delta\omega}{\omega_0}$$

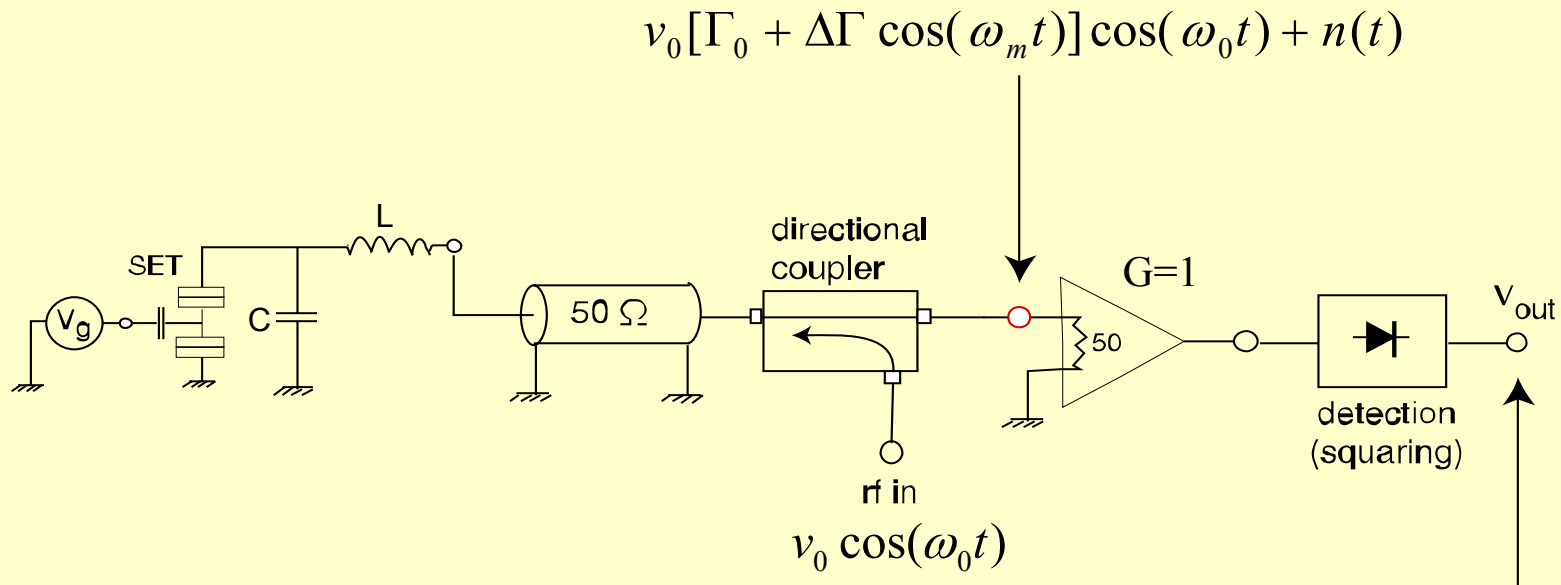
at resonance:

$$R_{eff} = \frac{L}{CR_{SET}} \equiv \frac{Z_T^2}{R_{SET}}$$

$$\Gamma = \frac{Z_{eff} - 50}{Z_{eff} + 50}$$



Signal-to-noise ratio



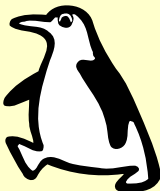
input noise $n(t)$ equivalent noise temp. T_0
 such that $S_V = k_B T Z_0$.

$$v_0 \frac{\Delta\Gamma}{2} \cos(\omega_m t) + n(t) \cos(\omega_0 t)$$

output noise $n(t) \cos(\omega_0 t)$

$$S_{V,output} = k_B T Z_0 / 2$$

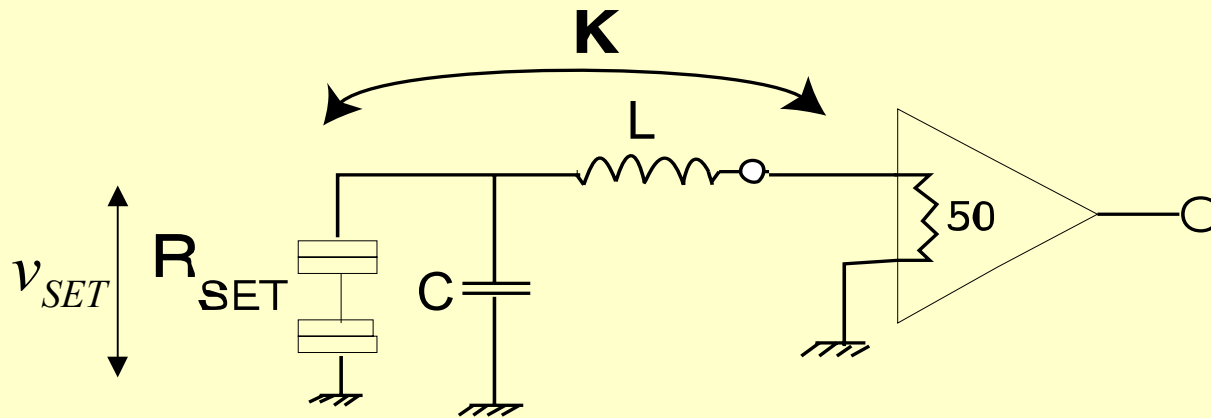
$$\frac{S}{N} = \frac{v_0 \Delta\Gamma}{\sqrt{4k_B T_0 Z_0}}$$



$$\frac{S}{N} = \frac{v_0 \Delta \Gamma}{\sqrt{4k_B T_0 Z_0}}$$

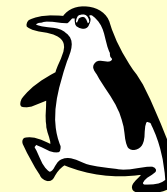
K: coupling of available power between impedances.
K=1 is conjugate matching

$$\Delta \Gamma = \frac{\partial |\Gamma|}{\partial q} \delta q$$



$$\frac{v_0^2}{2Z_0} \mathbf{K} = \frac{v_{SET}^2}{2R_{SET}}$$

$$\delta q_{RMS} = \frac{\sqrt{2k_B T_0 R_{SET} K}}{v_{SET} \frac{\partial |\Gamma|}{\partial q}}$$



Numerical estimation of charge and energy sensitivity.

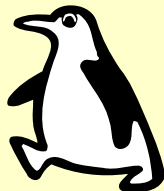
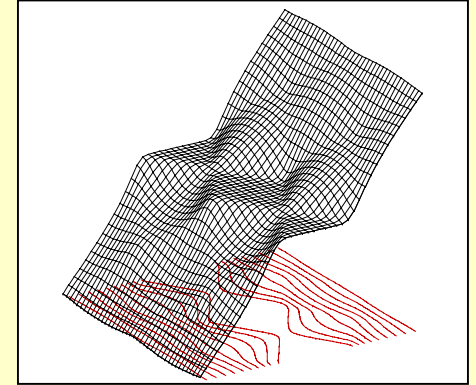
1) calculate $I(V_{\text{BIAS}}, V_{\text{GATE}})$ curves using orthodox theory.
Parameters E_C , T , R_{sigma} .

2) calculate $R(V_{\text{AC}}, V_{\text{GATE}})$ using

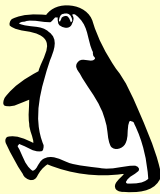
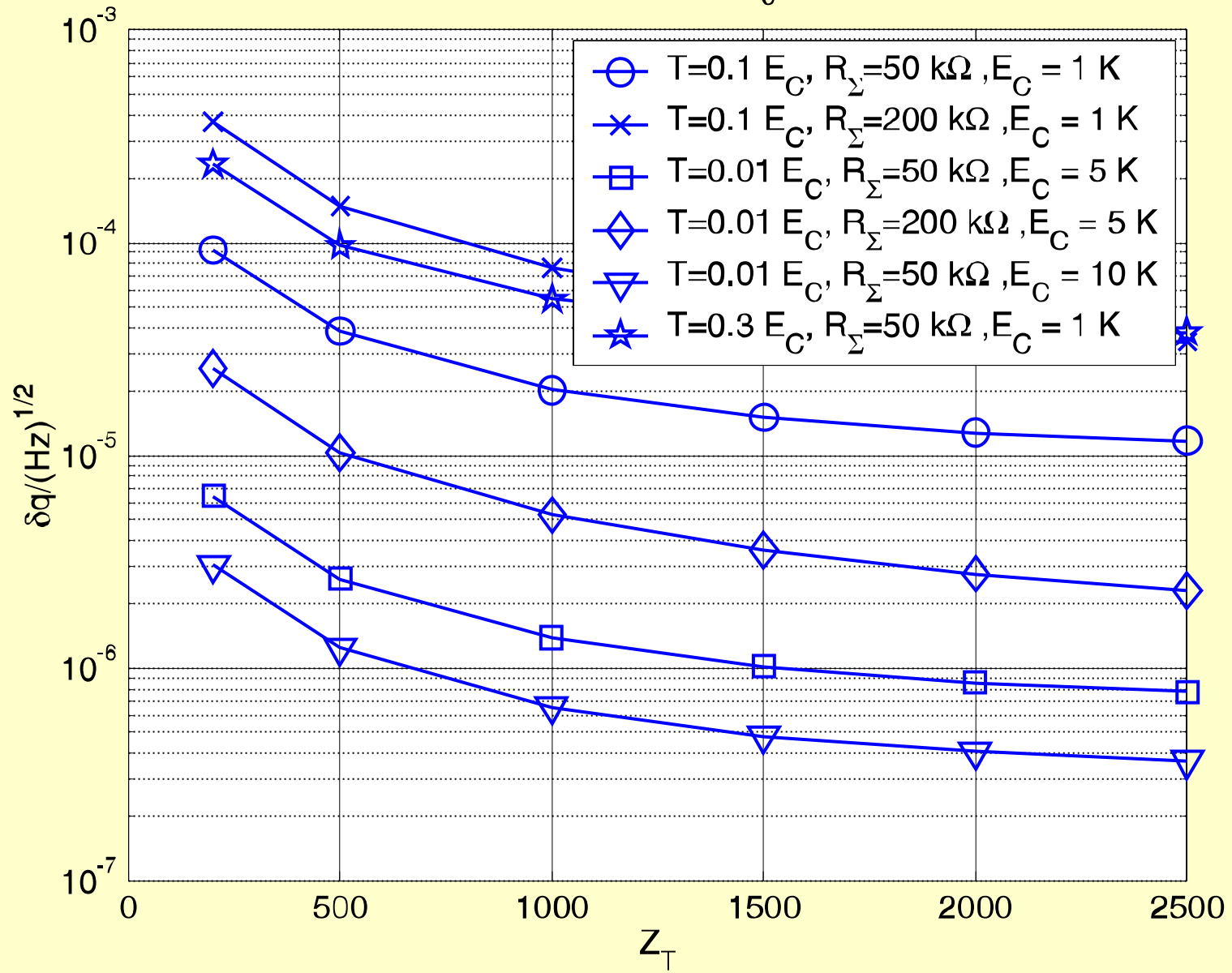
$$R \approx \sqrt{\frac{\langle U^2 \rangle}{\langle I^2 \rangle}}$$

3) minimize $\delta q_{\text{RMS}} = \frac{\sqrt{2k_B T_0 R_{\text{SET}} K}}{v_{\text{SET}} \frac{\partial |\Gamma|}{\partial q}}$ w.r.t. V_{AC} and V_{GATE}

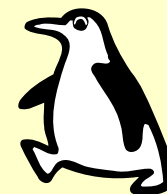
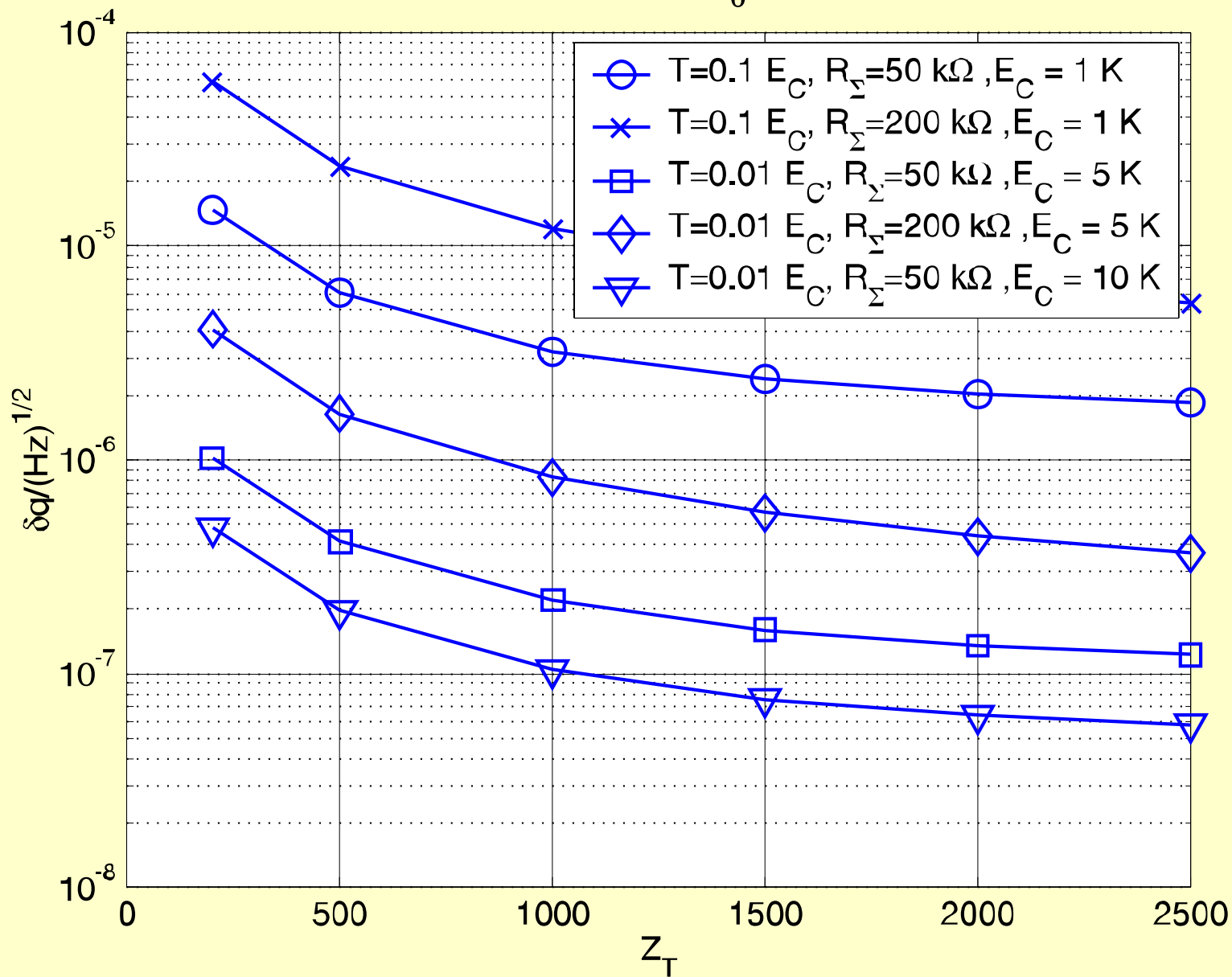
4) Results charge sensitivity **limited by amplifier**



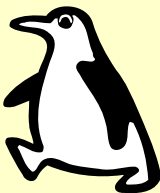
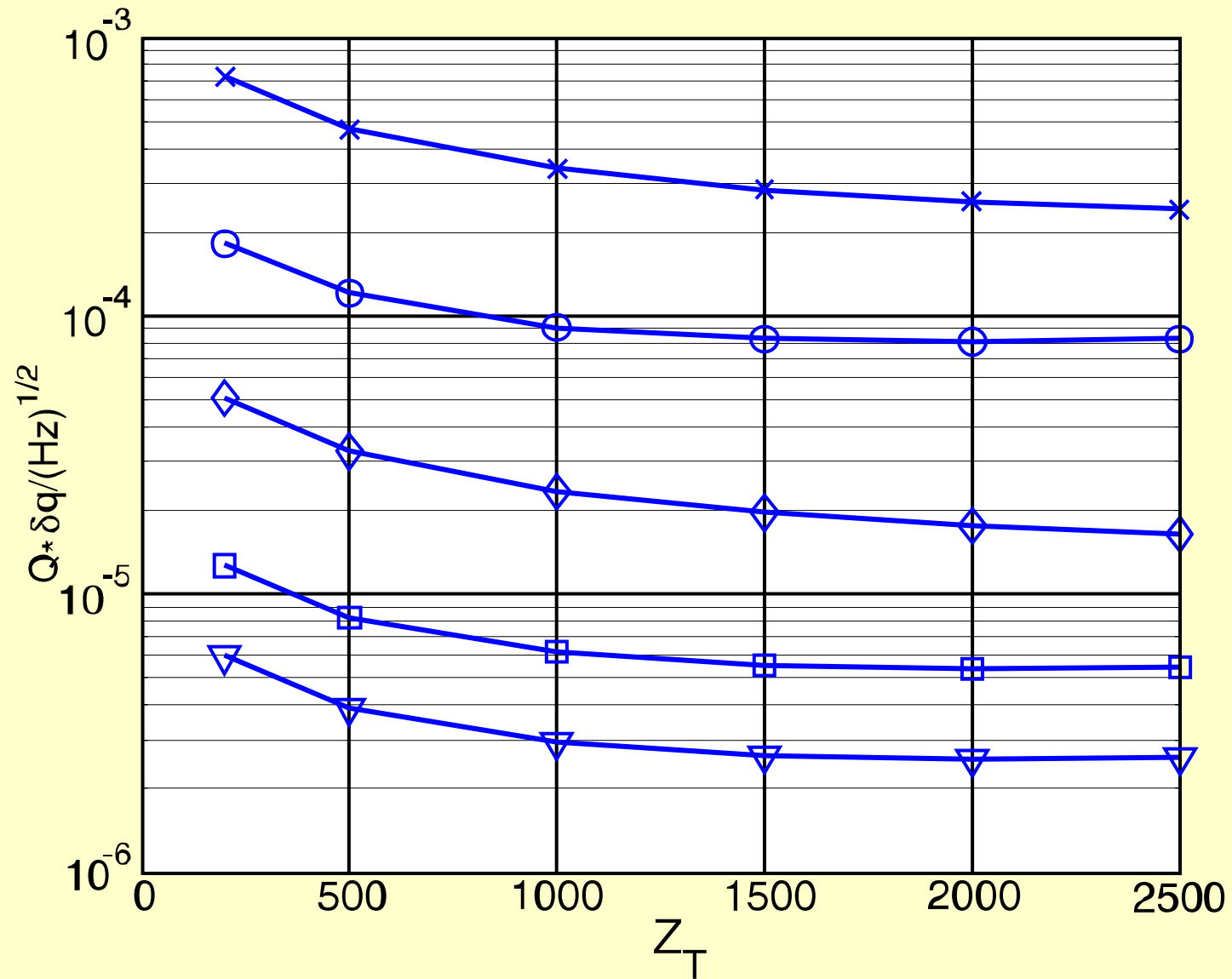
Charge sensitivity $T_0=4$ K



Charge sensitivity $T_0=100$ mK



Inverse gain-bandwidth product (lower is better)



Rule of thumb formula for charge sensitivity

$$\delta q \approx 1.46 \cdot 10^{-6} Z_T^{-0.91} t^{0.59} T_{EC}^{-1.01} R_\Sigma^{0.91} T_0^{0.5} [e / \sqrt{Hz}]$$

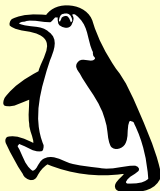
$$t = T / T_{EC}$$

$$Z_T = \sqrt{L / C}$$

amplifier noise

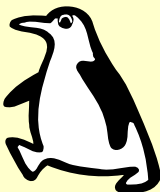
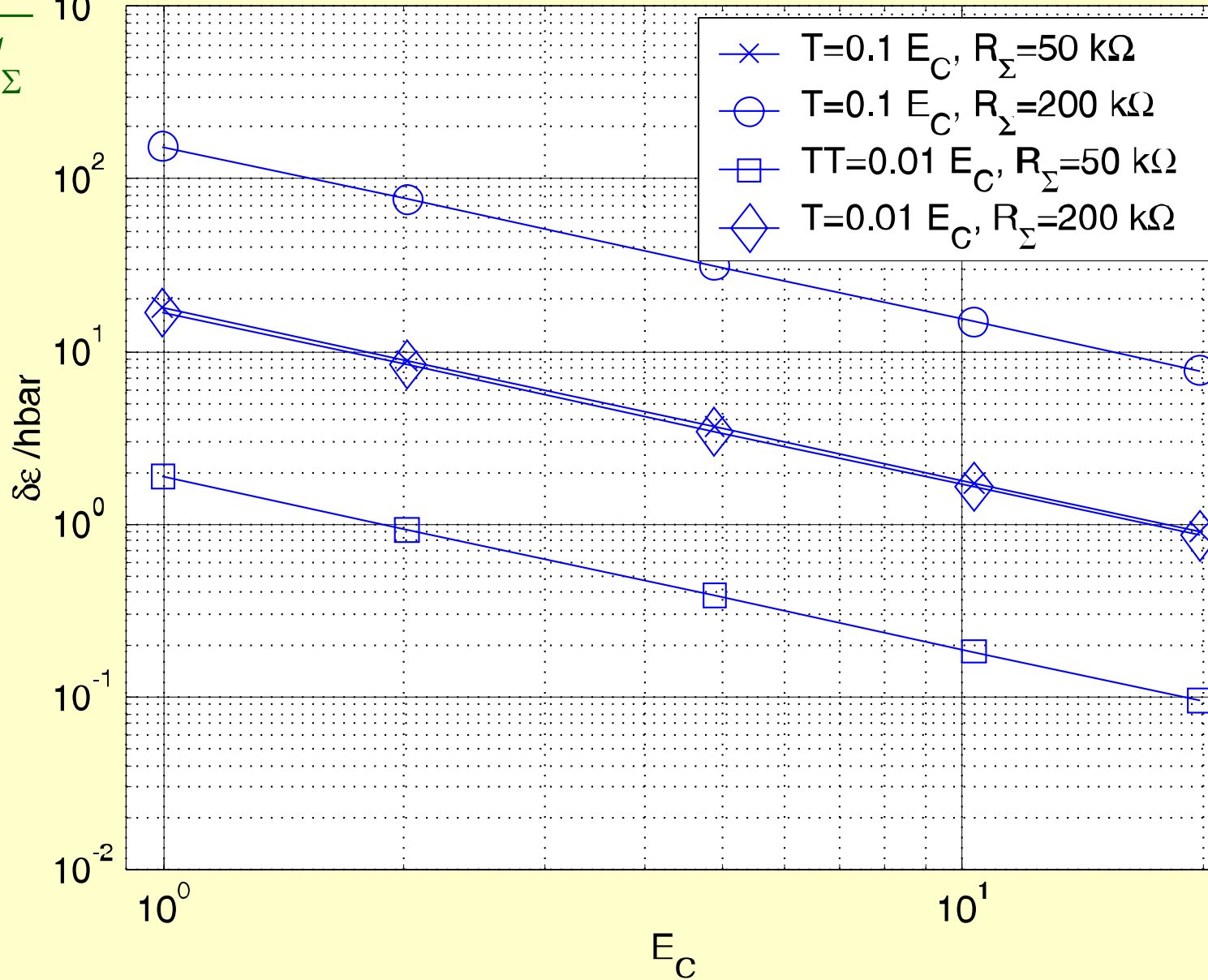
SET total resistance

charging energy in Kelvins



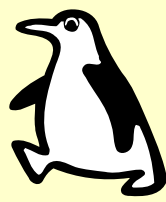
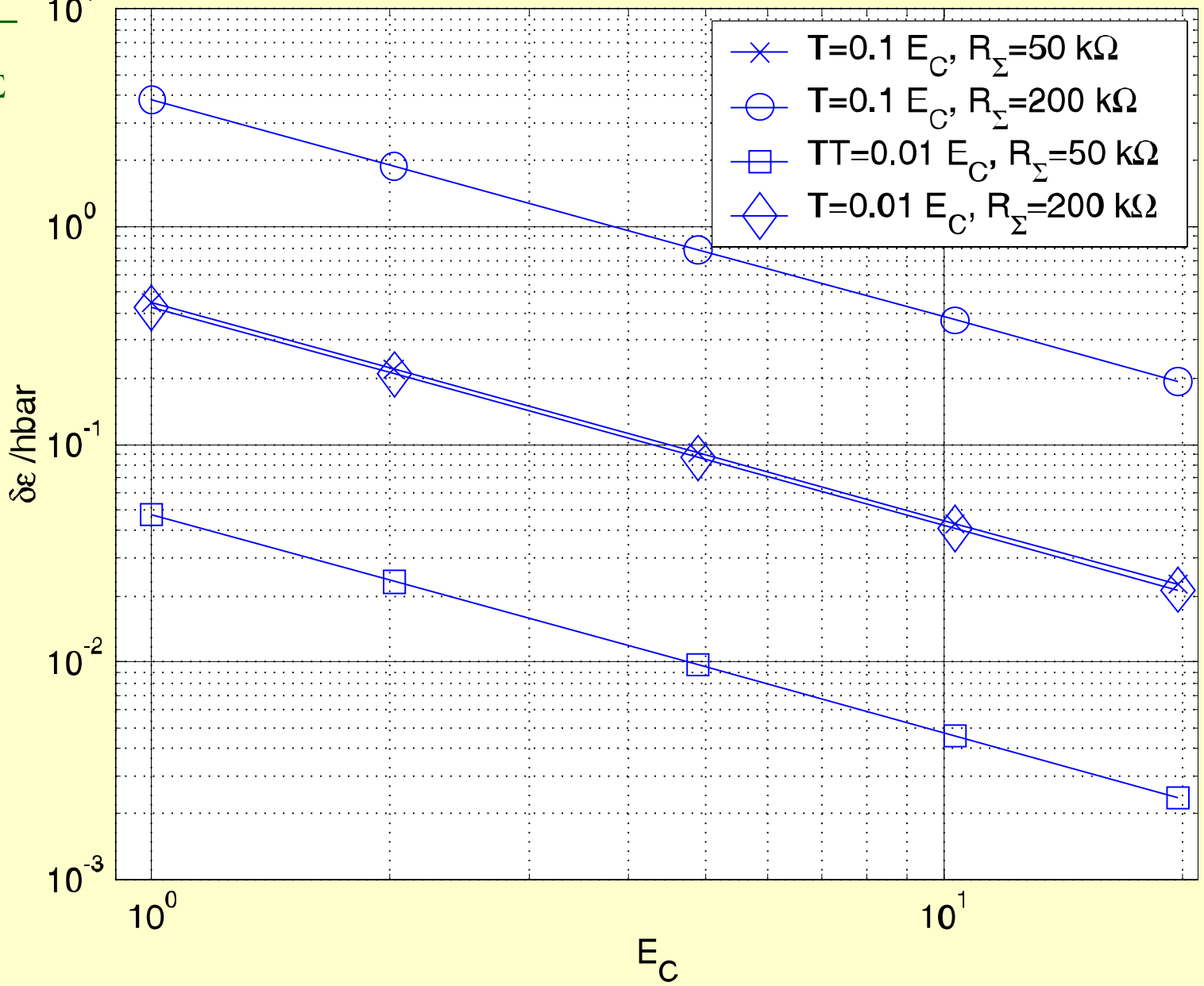
$$\delta\varepsilon = \frac{\delta q^2}{2C_\Sigma}$$

Island sensitivity $Z_T=2500 \Omega$, $T_0=4 \text{ K}$

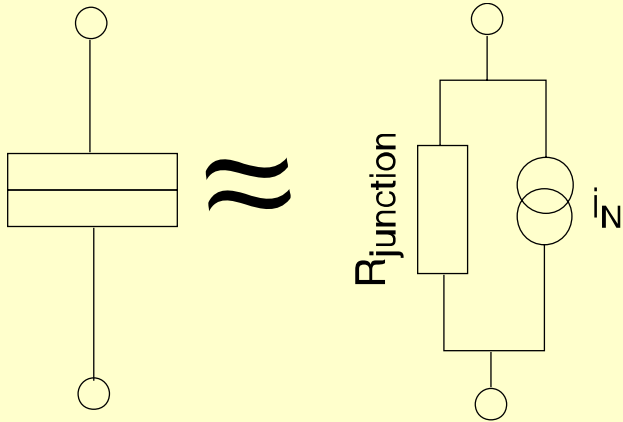


Island sensitivity $Z_T=2500 \Omega$, $T_0=100 \text{ mK}$

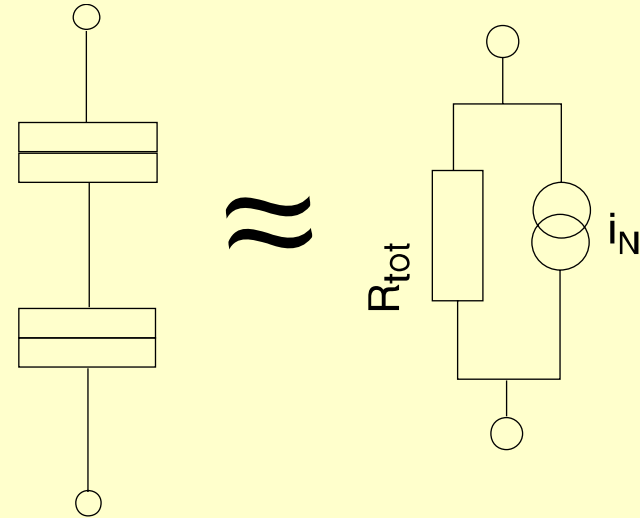
$$\delta\varepsilon = \frac{\delta q^2}{2C_\Sigma}$$



SET shot noise (as calibration standard)



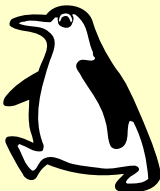
$$S_I = \frac{2eV}{R_{junction}} \coth \frac{eV}{2k_B T}$$



$$S_I = \frac{eV}{R_{tot}} \coth \frac{eV}{4k_B T}$$

assuming junctions uncorrelated

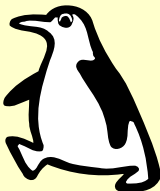
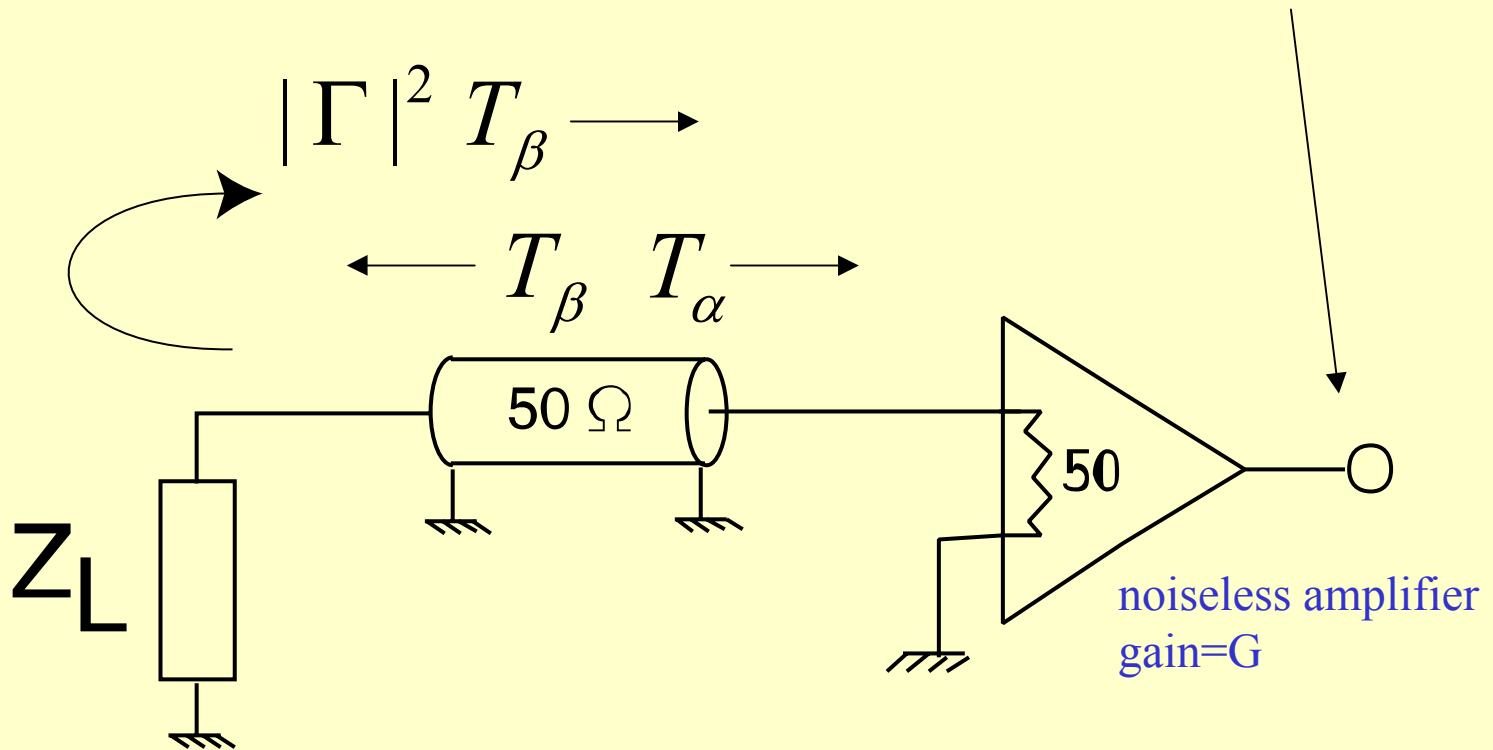
available power: $S_I R / 4$



NOISE POWER WAVES (=amplifier noise)

(correlation term)

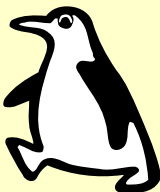
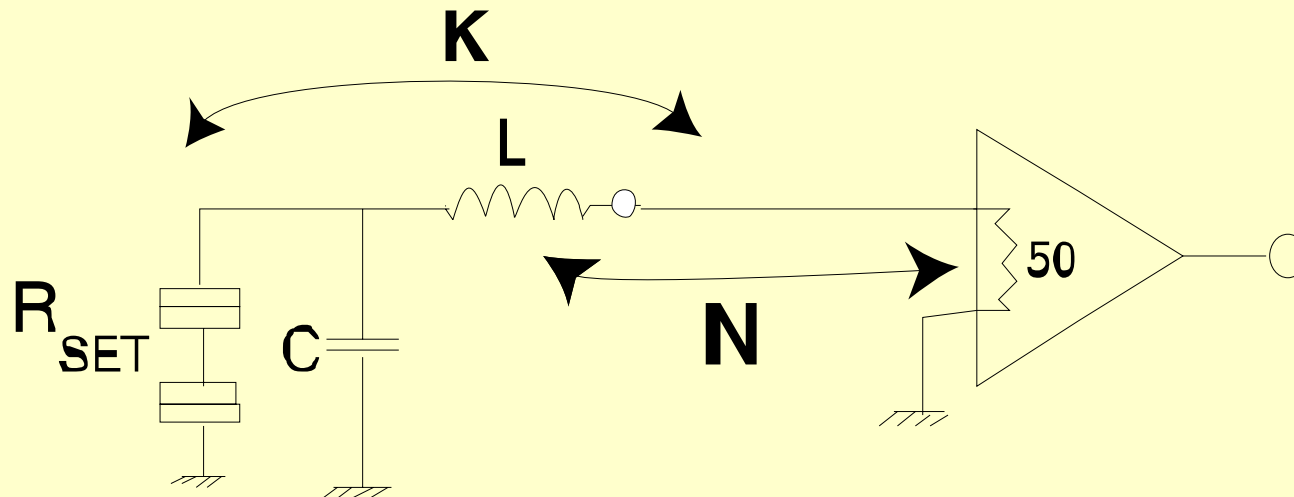
$$G \cdot \left\{ T_{\alpha} + |\Gamma|^2 T_{\beta} - 2 |\Gamma| T_{\gamma} \cos(\phi_{\gamma} + \phi_L) \right\}$$



Coupling of available power between objects

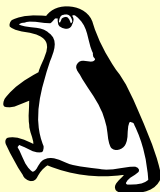
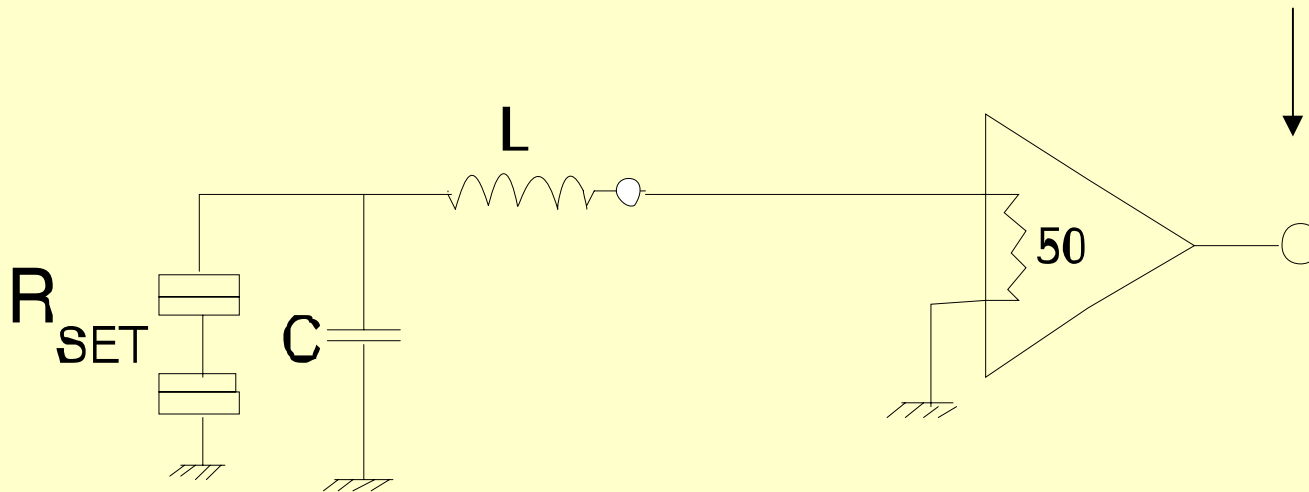
K: between SET and amplifier input

N: between LC tank circuit and amplifier input



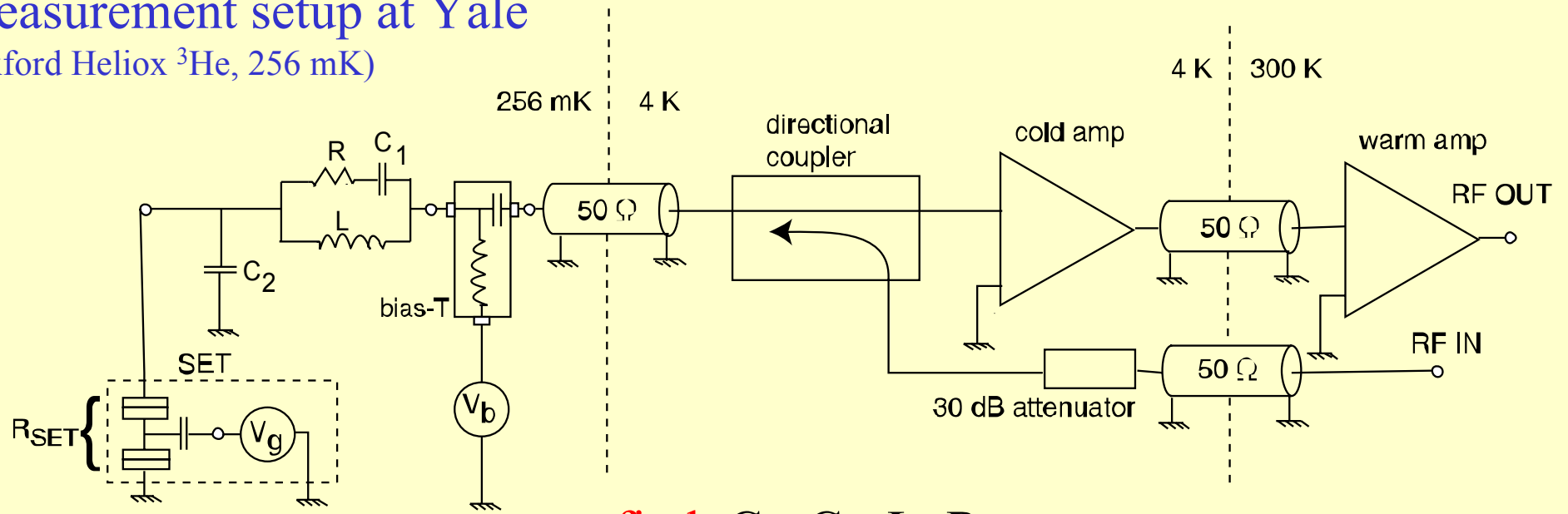
Measured total noise

$$G \cdot k_B \left\{ T_\alpha + |\Gamma|^2 T_\beta - 2|\Gamma| T_\gamma \cos(\phi_\gamma + \phi_L) + \mathbf{N} T_N + \mathbf{K} \frac{eV}{4k_B} \coth \frac{eV}{4k_B T} \right\}$$



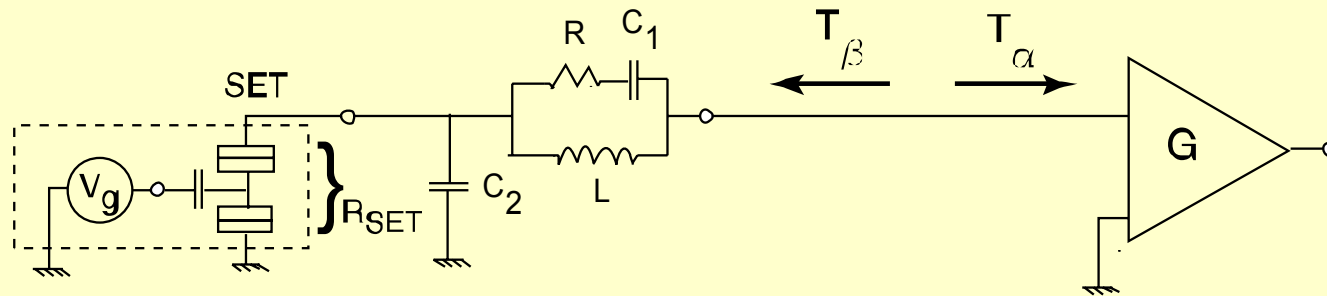
Measurement setup at Yale

(Oxford Heliox ^3He , 256 mK)

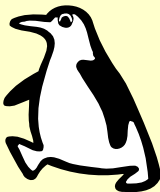


find: C_1, C_2, L, R

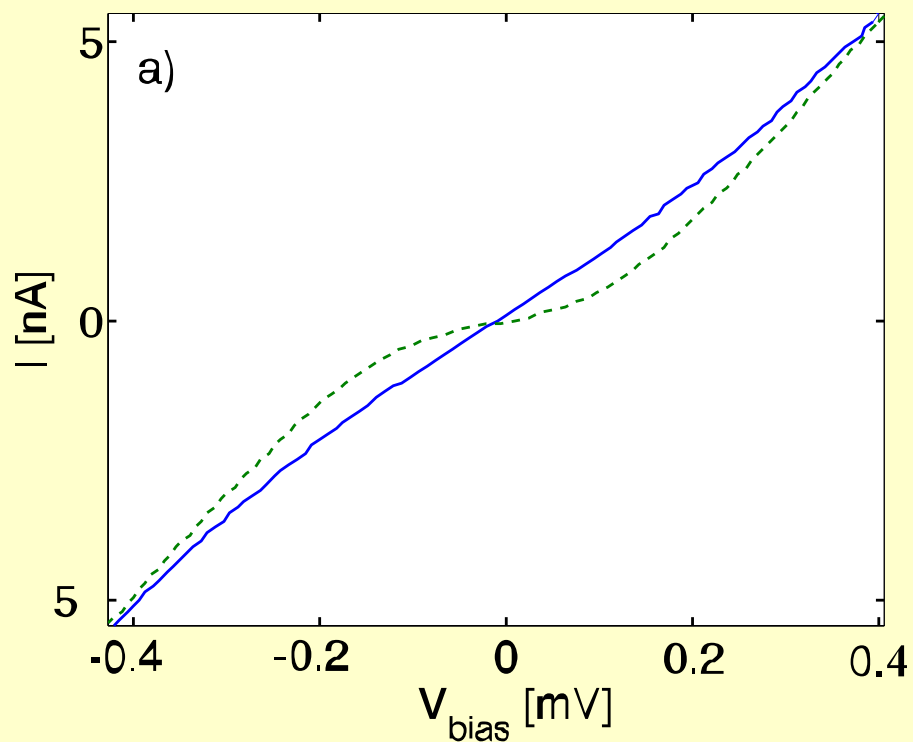
Equivalent noise setup



find: noise parameters

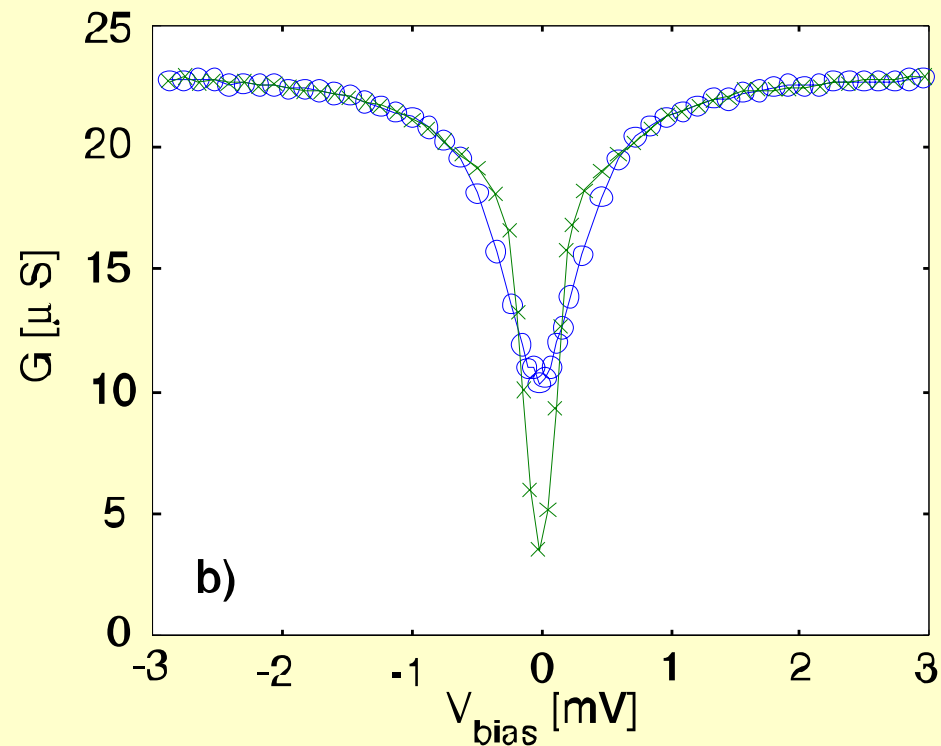


DC IV Curves



sample: Al SET

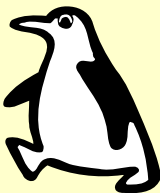
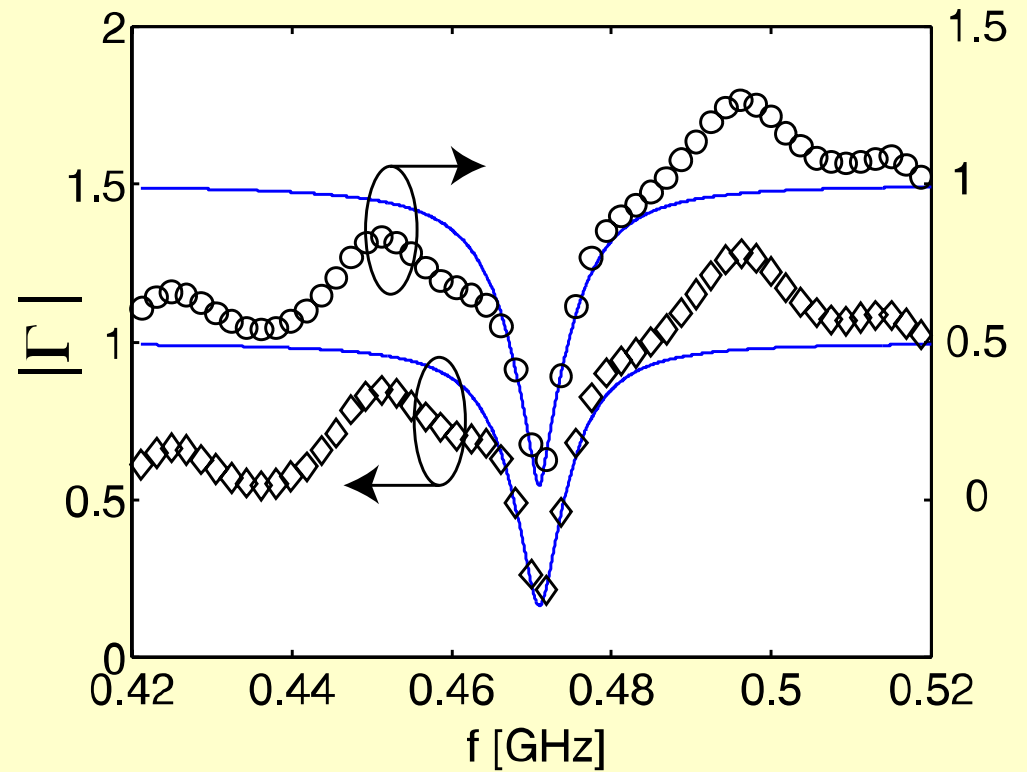
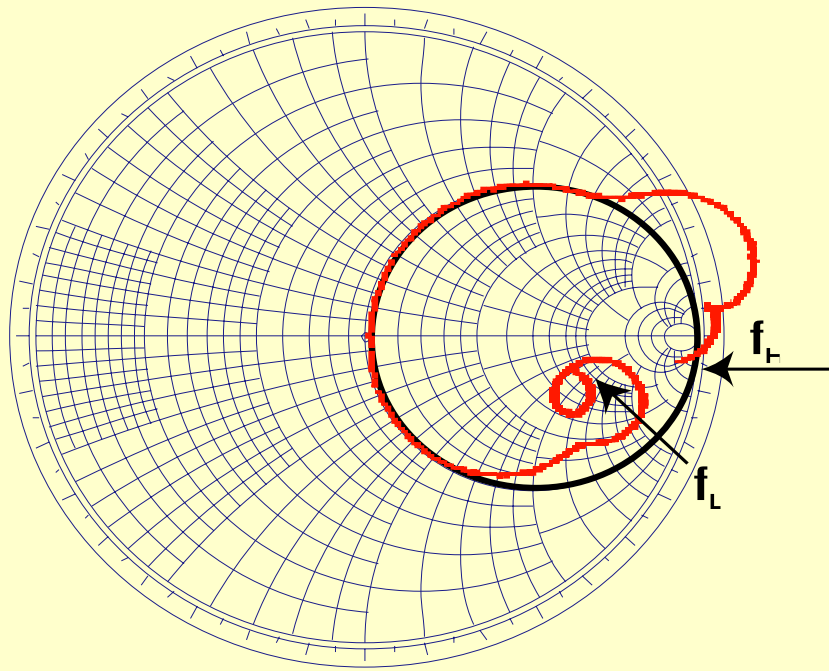
Conductance



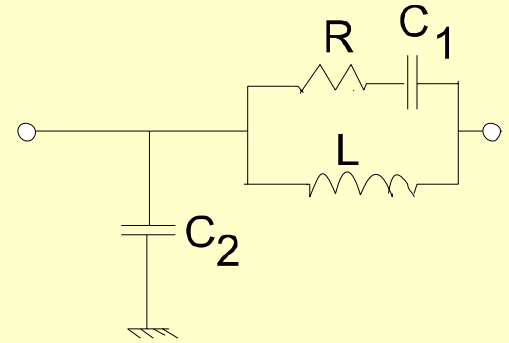
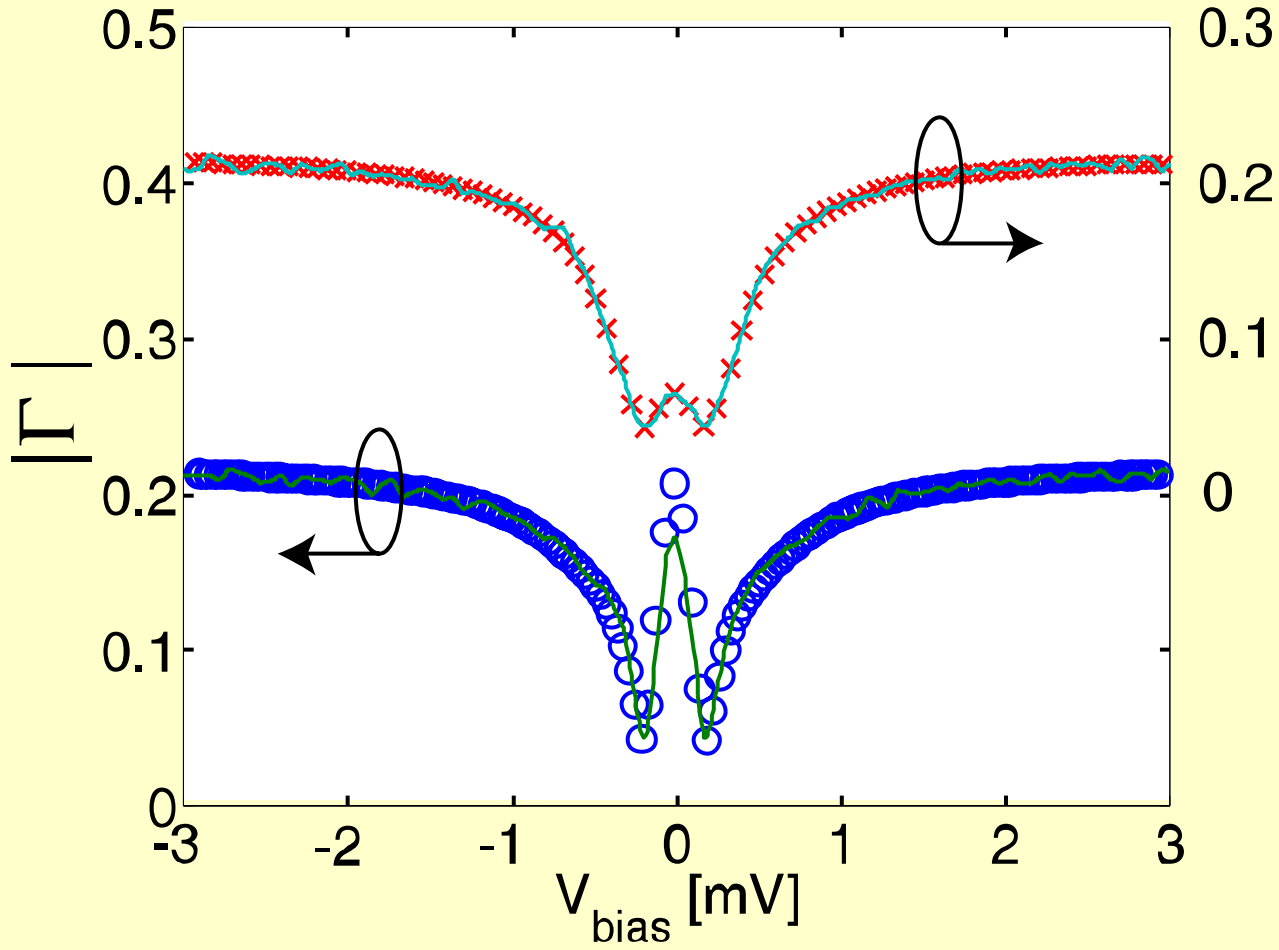
$\Rightarrow E_C = 1.13 \text{ K}$



Frequency response:



gamma vs. V_{bias}



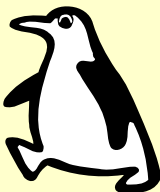
\Rightarrow

$$C_1 = 0.239 \text{ pF}$$

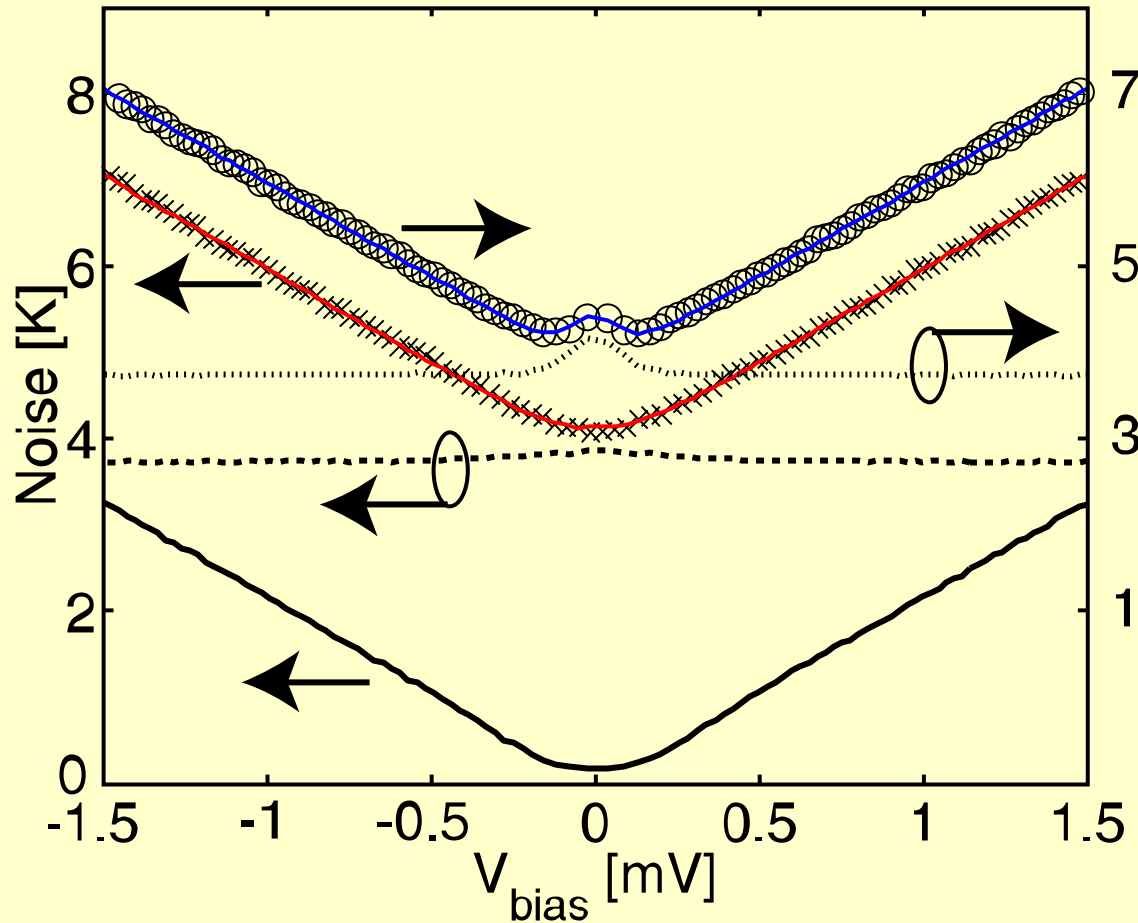
$$C_2 = 0.208 \text{ pF}$$

$$L = 256 \text{ nH}$$

$$R = 12.0 \text{ Ohm}$$



using C_1, C_2, L, R to fit noise parameters:



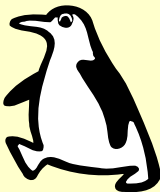
$$T_\alpha = 3.78$$

$$T_\beta = 1.22$$

$$T_\gamma = 0.35$$

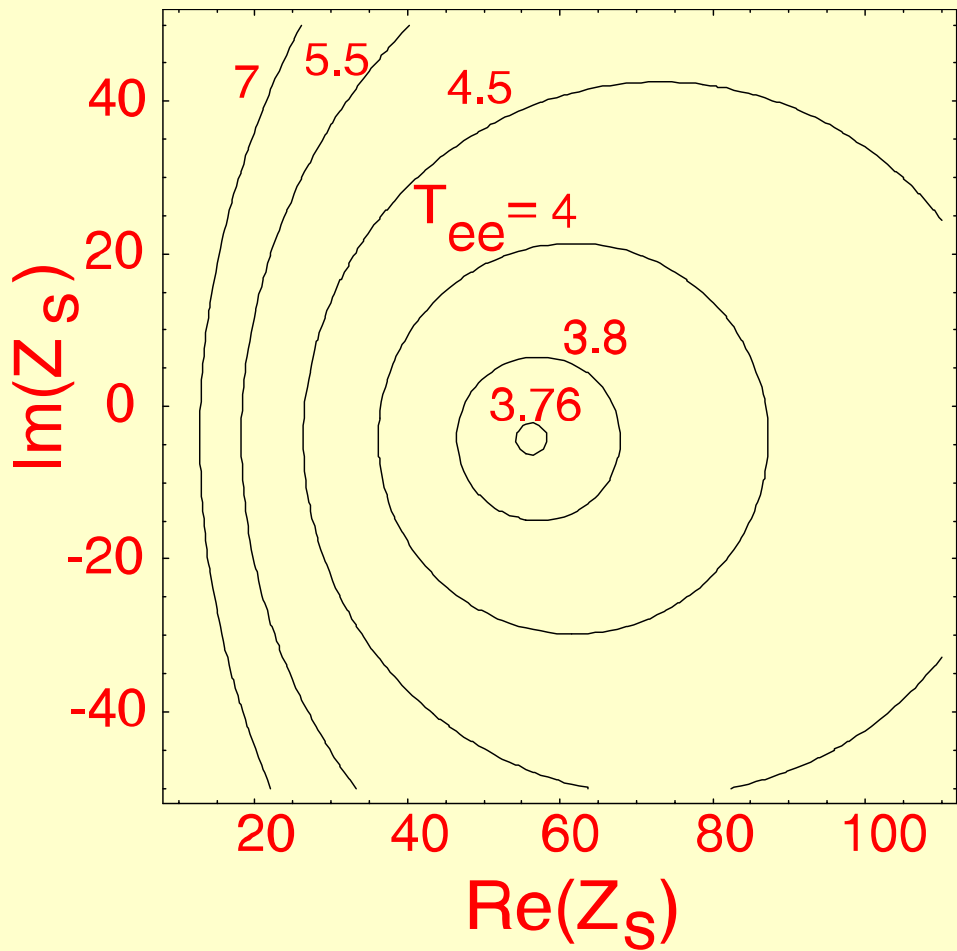
$$\phi_\gamma = 0.56$$

$$\Rightarrow T_0 \approx 4K$$

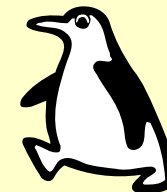
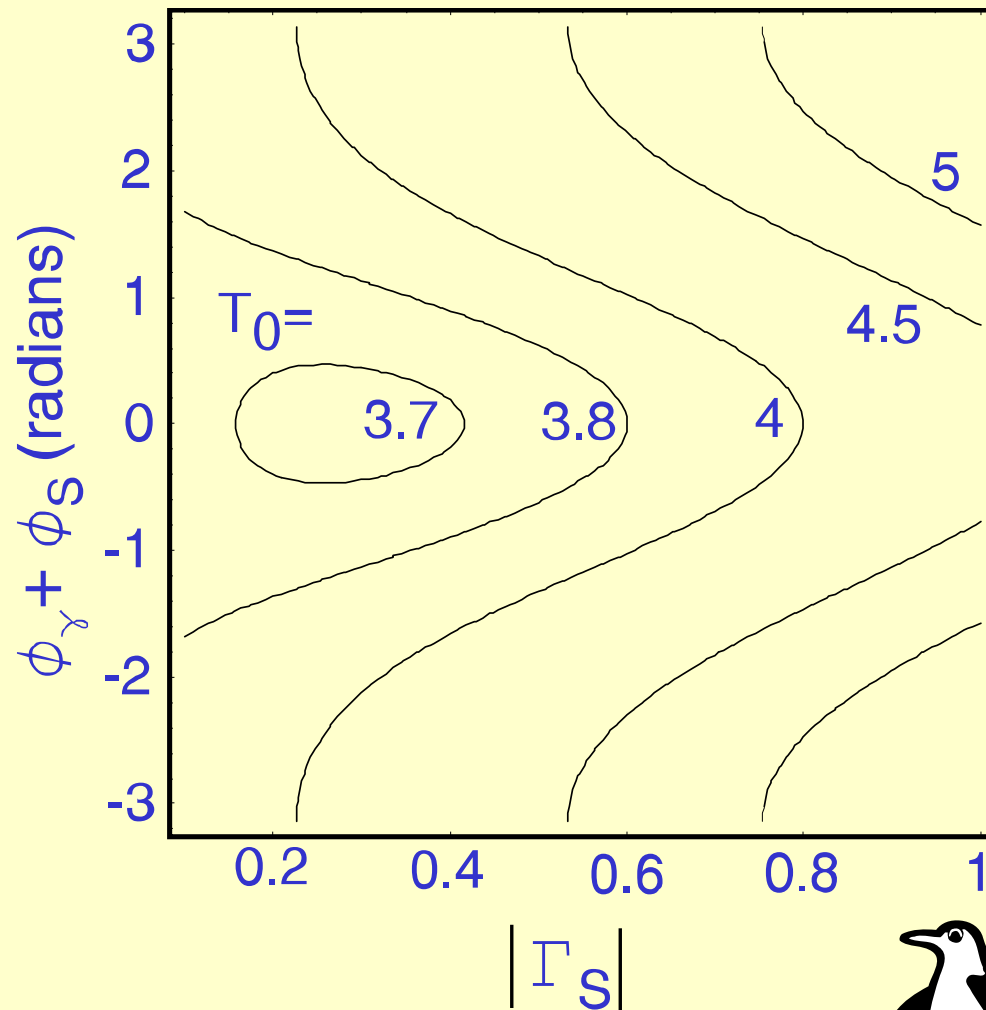


Amplifier noise contours

effective extended noise temperature



amplifier input noise temperature

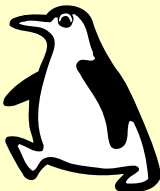


Comparison of $\delta q_{RMS} = \frac{\sqrt{2k_B T_0 R_{SET} K}}{v_{SET} \frac{\partial |\Gamma|}{\partial q}}$ to measured charge sensitivity.

extracted parameters: $R_{SET}, K, T_0, \Gamma(C_1, C_2, L, R, q)$

$$\Rightarrow \delta q_{calculated} = 3.5 \cdot 10^{-5} e / \sqrt{Hz}$$

$$\Rightarrow \delta q_{measured} = 3.8 \cdot 10^{-5} e / \sqrt{Hz}$$



Conclusion

- full model explaining rf-SET system
- estimation of charge sensitivity
- \Rightarrow lower noise amplifiers needed in order to reach shot-noise limit

$$\delta q_{RMS} = \frac{\sqrt{2k_B T_0 R_{SET} K}}{v_{SET} \frac{\partial |\Gamma|}{\partial q}}$$

$$\delta q \approx 1.46 \cdot 10^{-6} Z_T^{-0.91} t^{0.59} T_{EC}^{-1.01} R_{\Sigma}^{0.91} T_0^{0.5} [e / \sqrt{Hz}]$$

